

Production Analysis Decline Type Curves

Library of Decline Type Curves

Library of Decline Type Curves:

- **Fetkovich Type Curves — Radial Flow:**
 - **Original Fetkovich Decline Type Curve**
 - **"Rate Derivative" Decline Type Curve**
- **Fetkovich-McCray Type Curves — Radial Flow:**
 - **Fetkovich-McCray Type Curve**
 - **Fetkovich-Carter-McCray Type Curve (Gas)**
 - **Boundary Flux (do not use...)**
- **Fetkovich-McCray Curves — Fractured Wells:**
 - **Infinite Conductivity Vertical Fracture**
 - **Finite Conductivity Vertical Fracture**
- **Fetkovich-McCray Curves — Horizontal Wells**
- **Agarwal, et al. Methodology:**
 - **Radial Flow Case**
 - **Vertically Fractured Well Cases**
- **Crafton, et al. Methodology:**
 - **Rate normalization only...**

SPE 4629



Decline Curve Analysis Using Type Curves

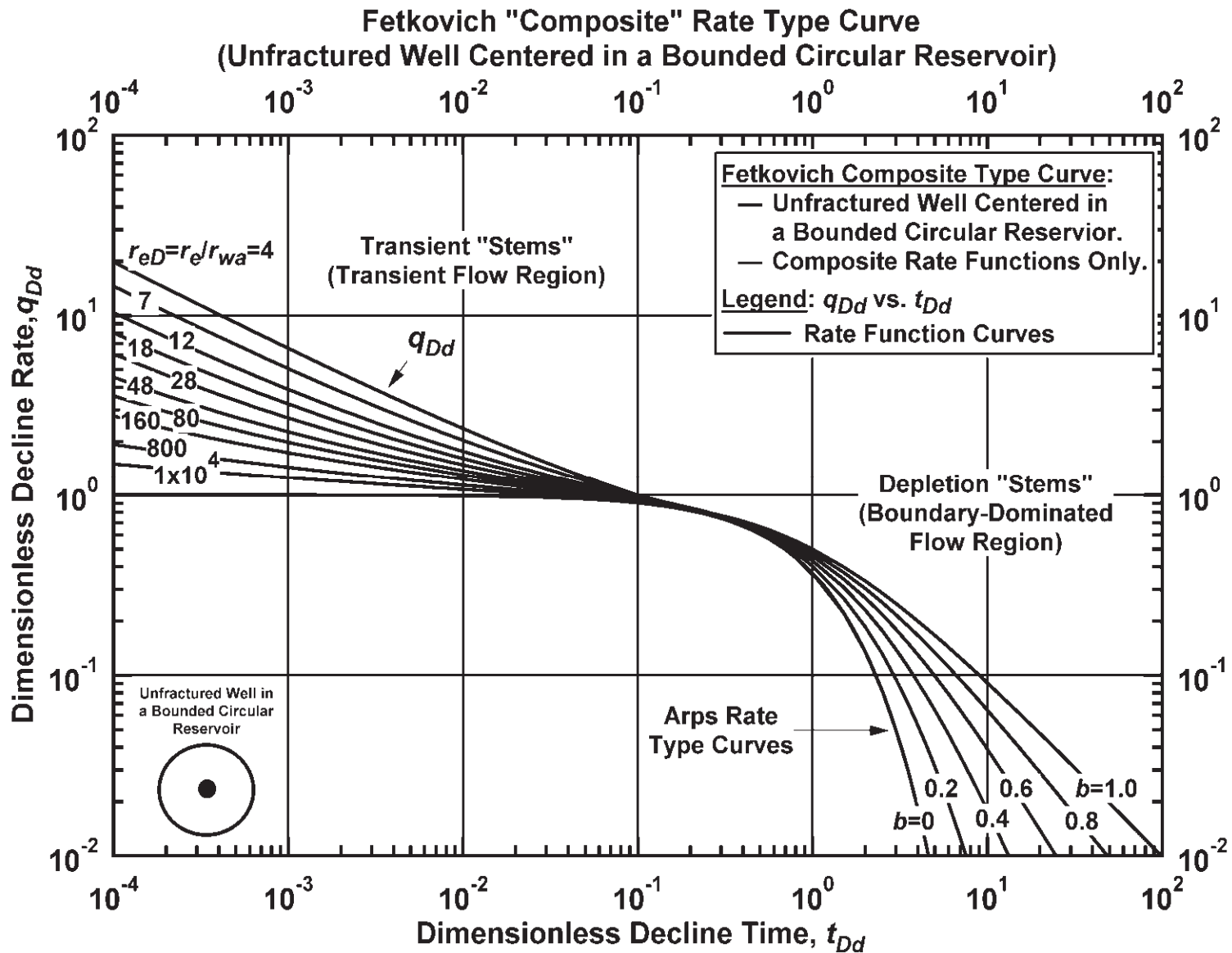
M.J. Fetkovich, SPE, Phillips Petroleum Co.

This paper demonstrates that decline curve analysis not only has a solid fundamental base but also provides a tool with more diagnostic power than has been suspected previously. The type curve approach provides unique solutions on which engineers can agree or shows when a unique solution is not possible with a type curve only.

JUNE 1980

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Fetkovich Decline Type Curve — Composite Curve



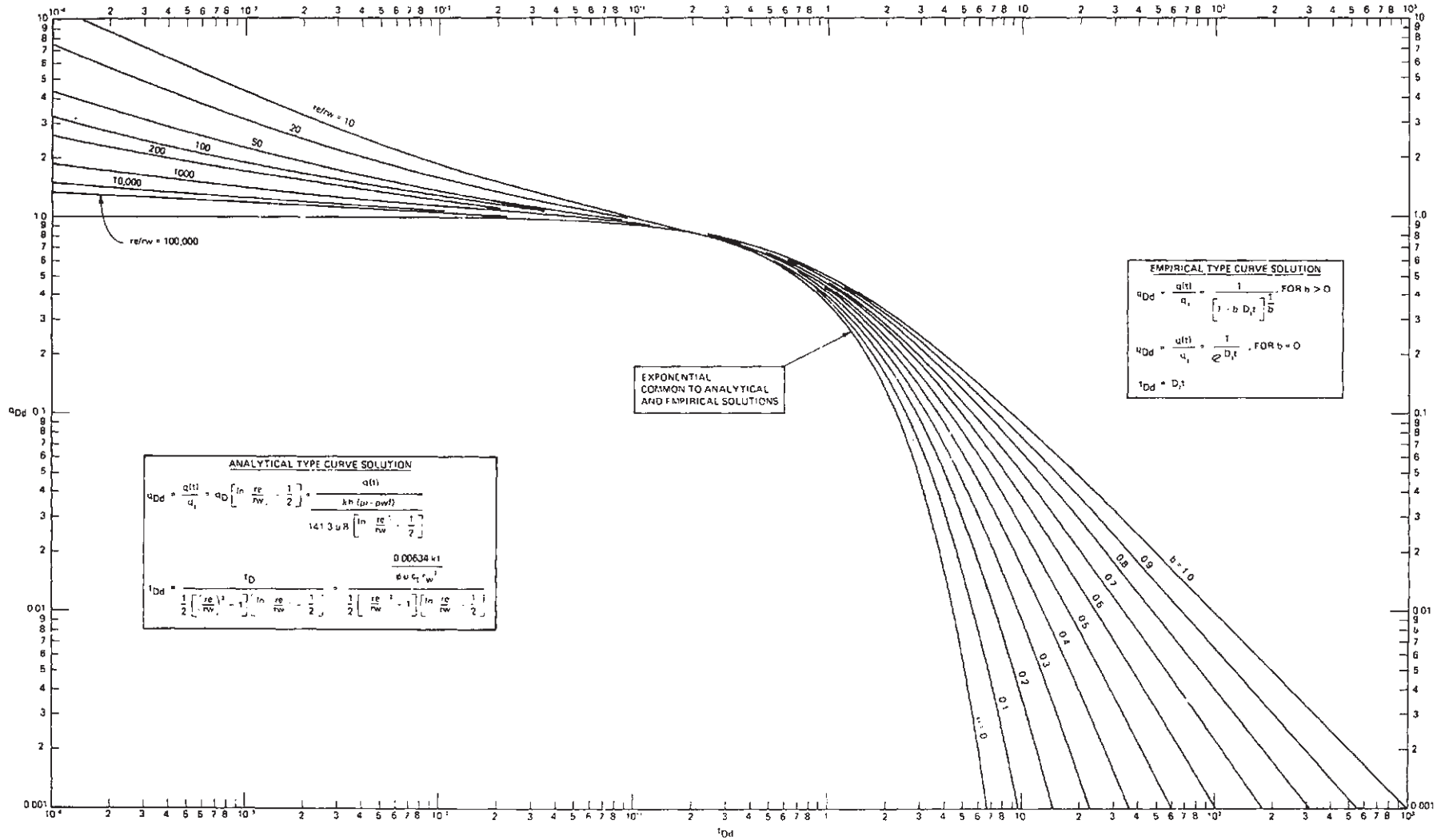
Fetkovich, M.J.: "Decline Curve Analysis Using Type Curves," JPT (June 1980) 1065-1077.

Discussion: Fetkovich "Composite" Decline Type Curve

- Assumes constant bottomhole pressure production.
- Radial flow in a finite radial reservoir system (single well).

Fetkovich Decline Type Curve — Composite Curve (original curve)

Fetkovich, M.J.: "Decline Curve Analysis Using Type Curves," JPT (June 1980) 1065-1077.



Composite of analytical and empirical type curves.

Discussion: Fetkovich "Composite" Decline Type Curve

- Reproduction of the original Fetkovich decline curve.

Fetkovich Decline Type Curve — Example Data Case (Well 13 — SPE 004629)

TABLE 3 — COMPARISONS OF kh DETERMINED FROM BUILDUP AND DECLINE CURVE ANALYSIS, FIELD A (SANDSTONE RESERVOIR); 160-ACRE SPACING, $r_e = 1,490$ ft, $r_w = 0.25$ ft

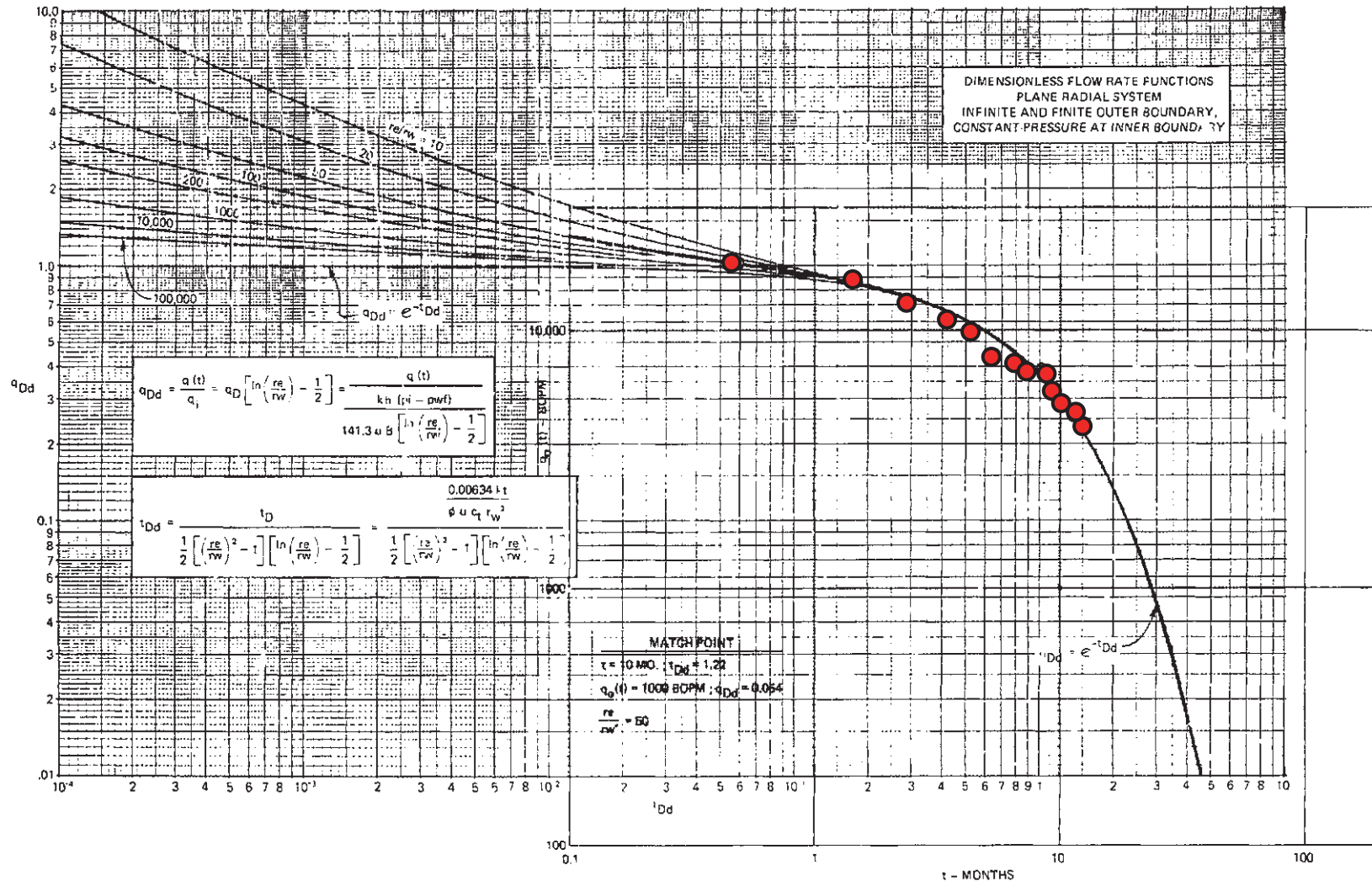
Well No.	h (ft)	ϕ (%)	S_{wc} (%)	Pressure Buildup Results			Decline Curve Analysis Results				
				Skin s	r_w' (ft)	kh (md-ft)	r_e/r_w' Matched	q_{Dd} (10,000 BOPM)	$\frac{\rho_i - \rho_{wt}}{(\mu_o B_o)}$	kh (md-ft)	k (md)
1	34	9.4	32.9	-0.23	0.3	120.5	*	0.52	6658	108	3.18
2	126	10.5	18.3	-2.65	3.5	56.7	*	0.68	7979	48	0.38
3	32	9.9	20.4	-3.71	10.3	63.0	*	0.43	8048	60	1.88
4	63	9.5	18.6	-3.41	7.6	28.5	40	0.58	8273	31	0.49
5	67	10.2	15.1	-4.29	18.3	44.4	20	0.57	6296	32	0.48
6	28	10.3	12.6	-2.07	2.0	57.9	*	0.60	7624	62	2.21
7	17	10.0	17.5	-3.41	7.6	16.8	10	1.30	7781	8.3	0.49
8	47	9.1	24.2	-3.74	10.6	16.6	10	1.14	7375	10	0.21
9	87	10.2	18.0	-4.19	16.5	104.7	*	0.435	5642	76	0.87
10	40	10.4	21.7	-5.80	82.9	363.2	*	0.36	1211	255	6.38
11	29	11.5	19.2	-1.00	2.0	59.9	*	0.56	7669	66	2.28
12	19	11.1	17.0	-3.97	13.3	8.9	50	3.30	5045	9.5	0.50
13	121	10.1	18.8	-3.85	11.8	47.5	50	0.54	7259	40.5	0.33
16	74	9.4	20.4	-4.10	15.0	224.8	*	0.32	5737	104	1.41
15	49	10.9	28.6	-3.59	9.1	101.9	*	0.43	4312	115	2.35
16	35	10.0	25.6	-4.57	24.2	14.3	20	0.96	5110	24	0.69
17	62	8.8	22.4	-3.12	5.7	27.2	*	0.82	8198	35	0.56
18	75	9.4	18.1	-1.50	1.2	65.1	*	0.52	6344	93	1.24
19	38	8.9	19.2	-2.11	2.1	40.5	20	0.54	6728	32	0.84
20	60	9.6	24.6	-5.48	60.1	88.1	*	0.345	5690	64	1.07
21	56	11.1	16.5	-2.19	2.2	39.1	20	0.72	5428	30	0.54
22	40	8.9	22.5	-3.79	11.1	116.0	100	0.46	8114	51	1.28

* r_w' used from buildup analysis with r_e of 1,490 ft.

Fetkovich, M.J.: "Decline Curve Analysis Using Type Curves." JPT (June 1980), 1065-1077.

Fetkovich Decline Type Curve — Example Data Case (Well 13 — SPE 004629)

Fetkovich, M.J.: "Decline Curve Analysis Using Type Curves," JPT (June 1980) 1065-1077.



Type-curve matching example for calculating Kh using decline curve data, Well 13, Field A.

Discussion: Fetkovich Example Match (SPE 004629)

- Lack of early time data is an omen of things to come.
- Late time data follow an exponential trend (constant p_{wf}).

Decline-Curve Analysis Using Type Curves—Case Histories

M.J. Fetkovich, SPE, Phillips Petroleum Co.

M.E. Vienot, SPE, Phillips Petroleum Co.

M.D. Bradley, SPE, Phillips Petroleum Co.

U.G. Kiesow, SPE, Phillips Petroleum Co.

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SPE Formation Evaluation, December 1987

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Fetkovich West Virginia Well A (SPE 013169)

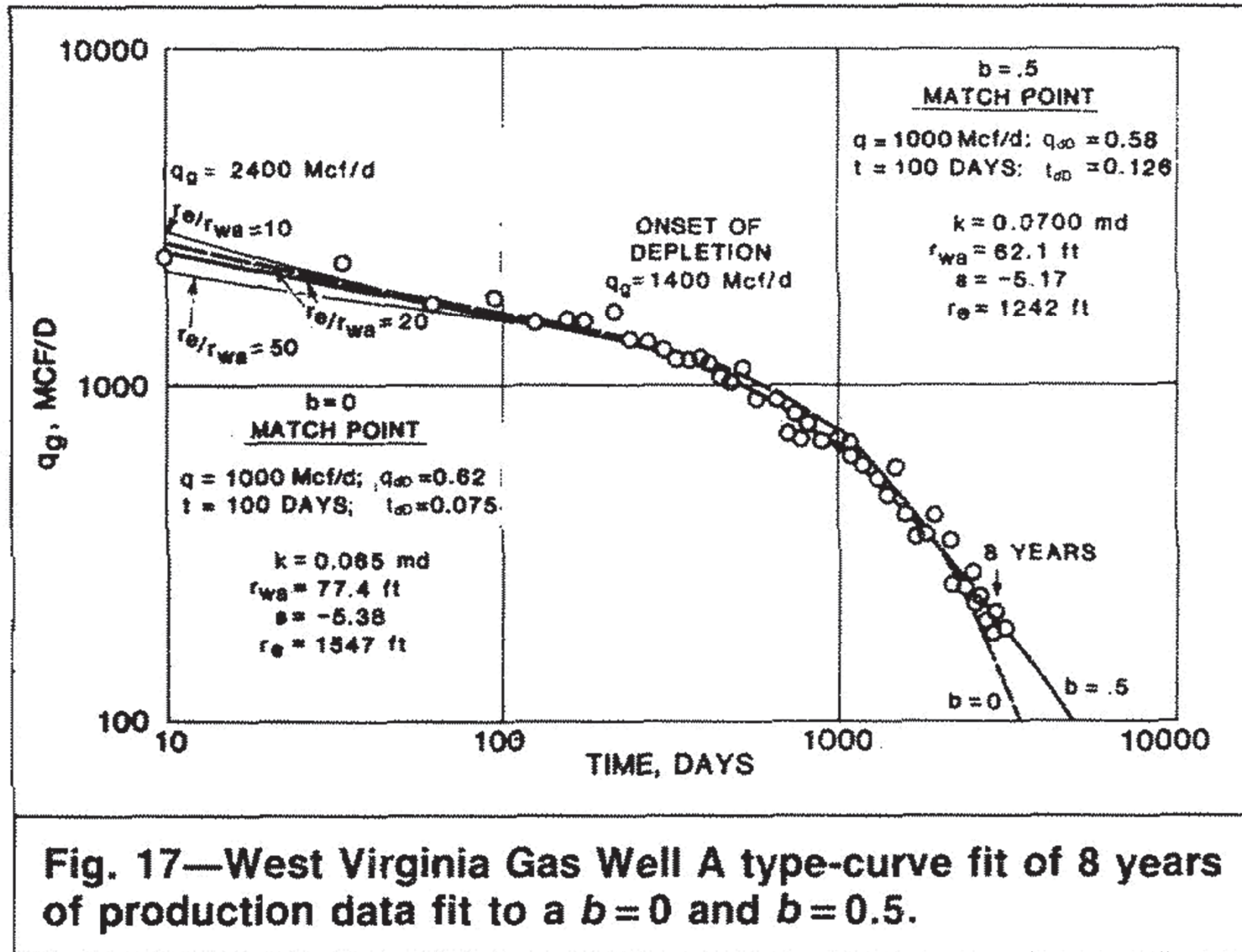


Fig. 17—West Virginia Gas Well A type-curve fit of 8 years of production data fit to a $b = 0$ and $b = 0.5$.

Fetkovich, M.J., Vienot, M.E., Bradley and M.D., Kiesow, U.G.: "Decline Curve Analysis Using Type Curves - Case Histories," SPEFE (Dec. 1987) 637-656.

Fetkovich West Virginia Well A (SPE 013169)

Fetkovich, M.J., Vienot, M.E., Bradley and M.D., Kiesow, U.G.: "Decline Curve Analysis Using Type Curves - Case Histories," SPEFE (Dec. 1987) 637-656.

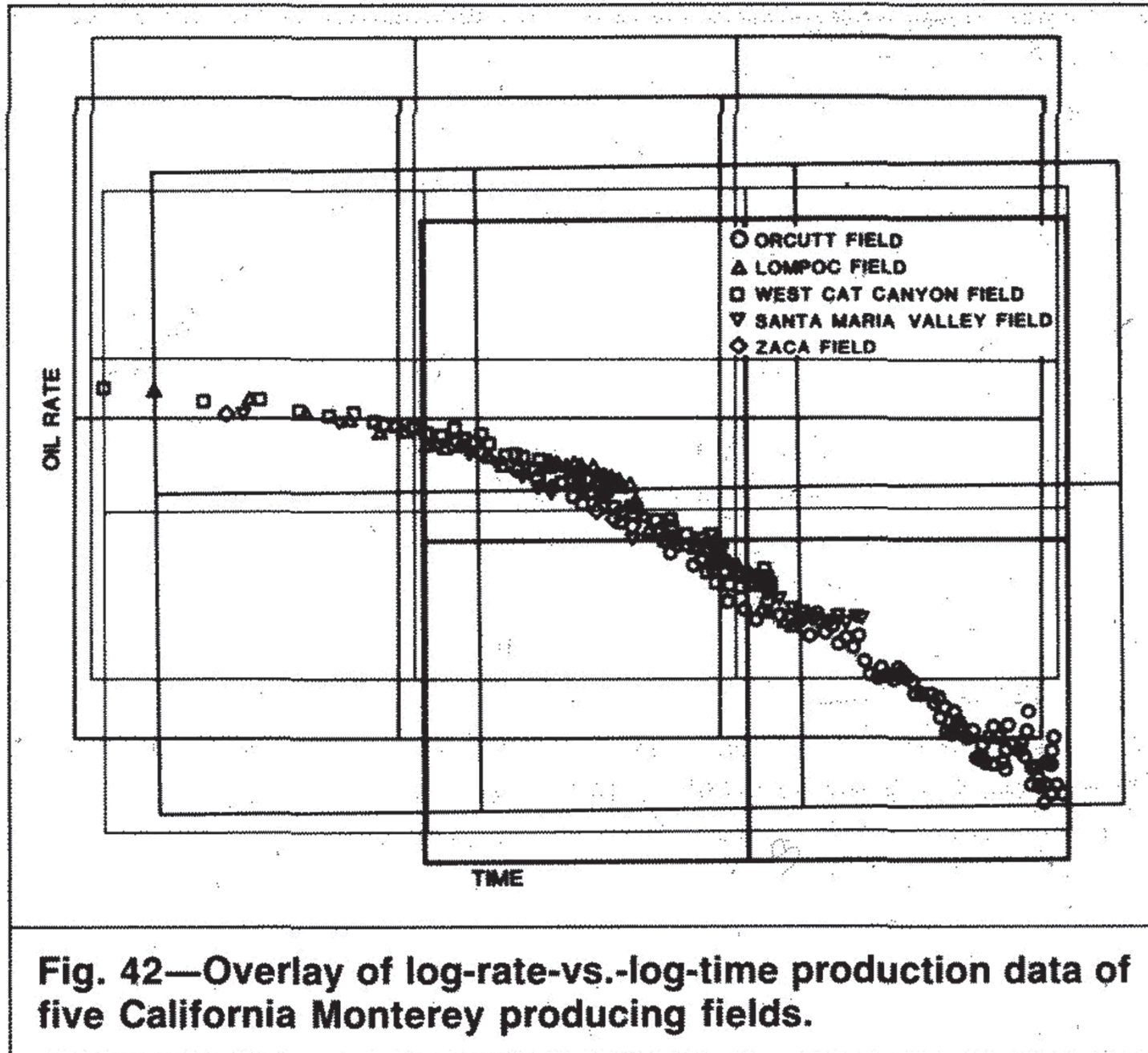
TABLE 3—WEST VIRGINIA GAS WELL A

Reservoir and Fluid Properties	
Gas specific gravity	0.57 (air = 1.00)
Porosity	0.06
Water saturation	0.35
Original pressure, psia	4,175
Pressure at start of decline, psia	3,268
Viscosity at 3,268 psia, cp	0.0171
System compressibility at 3,268 psia, psi^{-1}	177×10^{-6}
Thickness, ft	70
Temperature, °F	160
Wellbore radius, ft	0.354
Rate before 106-day pressure buildup, Mscf/D	2,181
Δp_p , psi^2/cp	774×10^6
B_g at 3,268 psia, scf/ft^3	208.8
B_g at 4,175 psia, scf/ft^3	253.9

TABLE 5—WEST VIRGINIA GAS WELL A: SUMMARY OF RATE-TIME ANALYSIS RESULTS

	Match Points			Horner Analysis
	Composite Type Curve $b = 0$	Composite Type Curve $b = 0.5$	Carter Type Curve $\lambda = 0.55$ ($b = 0.5$)	
q_{dD}	0.62	q_{dD} 0.58	q_{DR} 0.24	
t_{dD}	0.075	t_{dD} 0.126	t_{DR} 60	
$q(t)$, Mscf/D	1,000	$q(t)$, Mscf/D 1,000	$q(t)$, Mscf/D 1,000	
t , days	100	t , days 100	t , days 100	
	$r_e/r_{wa} = 10$	$r_e/r_{wa} = 20$	$r_e/r_{wa} = 50$	
	$b = 0$ Evaluation			
kh , md-ft	3.292	4.558	6.231	
k , md	0.047	0.065	0.089	0.0805
r_{wa} , ft	154.7	77.4	30.9	
s	-6.08	-5.38	-4.47	-5.52
r_e , ft	1,547	1,547	1,547	
	$b = 0.5$ Evaluation			
kh , md-ft	3.542	4.902	6.705	
k , md	0.0506	0.0700	0.0958	
r_{wa} , ft	124.2	62.1	24.8	
s	-5.86	-5.17	-4.25	
r_e , ft	1,242	1,242	1,242	
	Carter's $\lambda = 0.55$ Evaluation			
kh , md-ft	3.451	4.746	6.699	
k , md	0.0493	0.0678	0.0957	
r_{wa} , ft	126.4	62.6	24.8	
s	-5.88	-5.17	-4.25	
r_e , ft	1,264	1,252	1,240	

Fetkovich Monterey Wells (SPE 013169)



Fetkovich, M.J., Vienot, M.E., Bradley and M.D., Kiesow, U.G.: "Decline Curve Analysis Using Type Curves - Case Histories," SPEFE (Dec. 1987) 637-656.



SPE 21513

Decline Curve Analysis for Variable Pressure Drop/Variable Flowrate Systems

by T.A. Blasingame, T.L. McCray, and W.J. Lee, Texas A&M U.

SPE 25909

Decline-Curve Analysis Using Type Curves--Analysis of Gas Well Production Data

by J.C. Palacio, ECOPETROL(Colombia)/Texas A&M U. and T.A. Blasingame, Texas A&M U.

This is a preprint -- subject to correction.
19 October 1994



SPE 28688

Decline Curve Analysis Using Type Curves--Analysis of Oil Well Production Data Using Material Balance Time: Application to Field Cases

by L.E. Doublet,* Texas A&M U., P.K. Pande,* Fina Oil and Chemical Company, T.J. McCollum,* UNOCAL-Coastal California, and T.A. Blasingame,* Texas A&M U.

* SPE Members

Auxiliary Plotting Functions (Theory)

Q. What are the "auxiliary" plotting functions for PA?

A. Time (or material balance time)-averaged pressure drop and flowrate functions — "integral" and "integral-derivative" forms are used.

Normalized Pressure Drop:

- "Pressure Derivative"

$$\left[\frac{\Delta p}{q_o} \right]_d = \bar{t} \frac{d}{d\bar{t}} \left[\frac{\Delta p}{q_o} \right]$$

- "Pressure Integral"

$$\left[\frac{\Delta p}{q_o} \right]_i = \frac{1}{\bar{t}} \int_0^{\bar{t}} \left[\frac{\Delta p}{q_o} \right] d\bar{t}$$

- "Pressure Integral-Derivative"

$$\left[\frac{\Delta p}{q_o} \right]_{id} = \bar{t} \frac{d}{d\bar{t}} \left[\left[\frac{\Delta p}{q_o} \right]_i \right]$$

Normalized Flowrate:

- "Rate Derivative"

$$\left[\frac{q_o}{\Delta p} \right]_d = \bar{t} \left| \frac{d}{d\bar{t}} \left[\frac{q_o}{\Delta p} \right] \right|$$

- "Rate Integral"

$$\left[\frac{q_o}{\Delta p} \right]_i = \frac{1}{\bar{t}} \int_0^{\bar{t}} \left[\frac{q_o}{\Delta p} \right] d\bar{t}$$

- "Rate Integral-Derivative"

$$\left[\frac{q_o}{\Delta p} \right]_{id} = \bar{t} \left| \frac{d}{d\bar{t}} \left[\left[\frac{q_o}{\Delta p} \right]_i \right] \right|$$

Theory:

The auxiliary functions (specifically the integral and integral derivative functions) are designed to provide "smooth" data functions – which should improve interpretation and analysis.

Application:

- "Pressure drop" functions → "Normalized PI" plot .
- "Flowrate" functions → "Blasingame" plot .

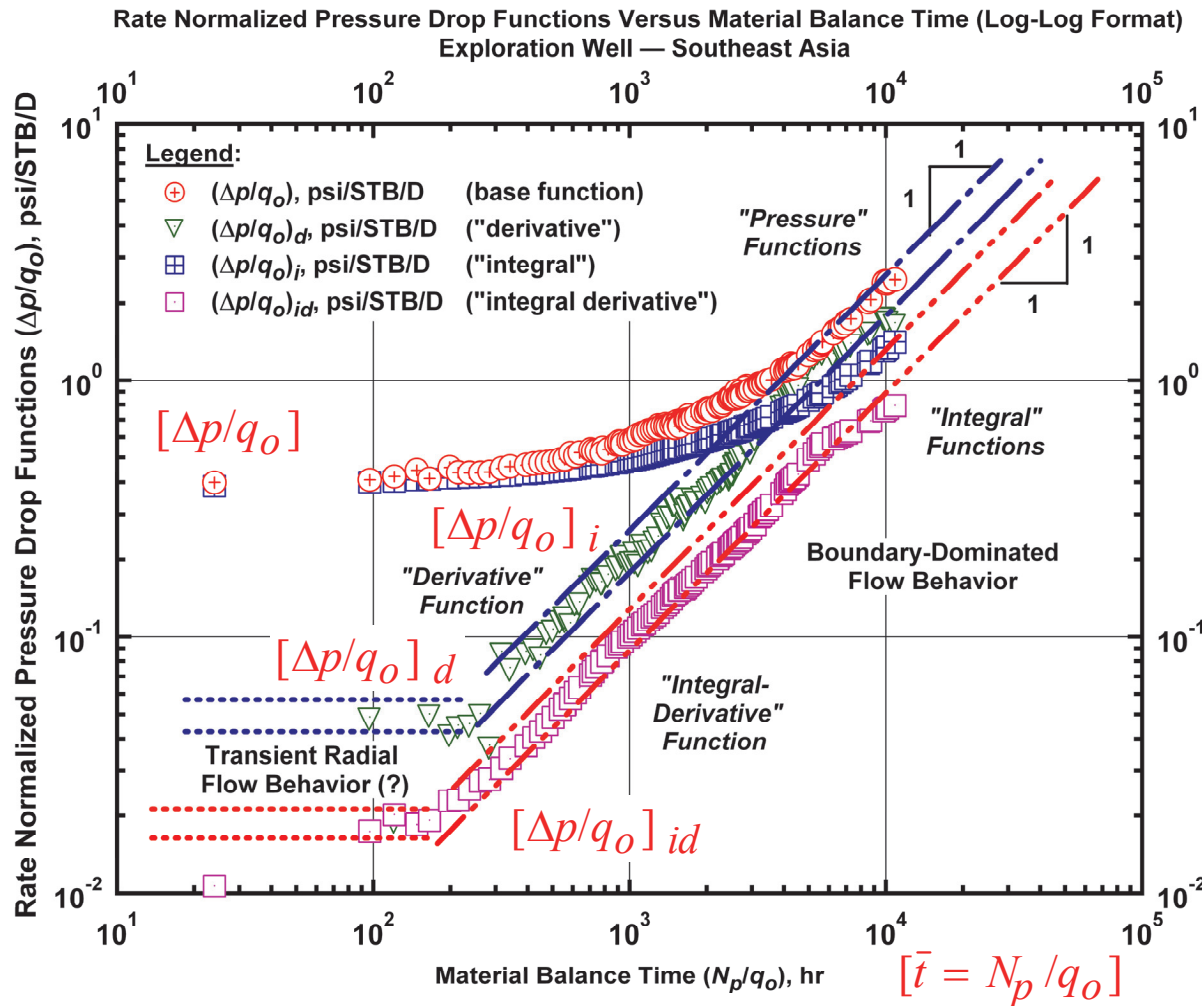
Discussion: Modern PA — Auxiliary Plotting Functions (Theory)

- *Theory for auxiliary plotting functions?* (just calculus ...)
- *Purpose of auxiliary plotting functions?* (more resolution for PA data)
- *Advice?* (use **BOTH** pressure drop and flowrate functions (separate plots))

Auxiliary Plotting Functions (Application 1)

Q. Application 1 — What is the "Normalized PI" plot?

A. Pressure drop auxiliary functions versus material balance time.



Theory:

$(\Delta p/q_o)$ fcns versus N_p/q_o :

$$\bar{t} = \frac{N_p}{q_o}$$

$$\left[\frac{\Delta p}{q_o} \right]_d = \bar{t} \frac{d}{d\bar{t}} \left[\frac{\Delta p}{q_o} \right]$$

$$\left[\frac{\Delta p}{q_o} \right]_i = \frac{1}{\bar{t}} \int_0^{\bar{t}} \left[\frac{\Delta p}{q_o} \right] d\bar{t}$$

$$\left[\frac{\Delta p}{q_o} \right]_{id} = \bar{t} \frac{d}{d\bar{t}} \left[\left[\frac{\Delta p}{q_o} \right]_i \right]$$

Application:

Analysis approach same as PTA — look for characteristic behavior.

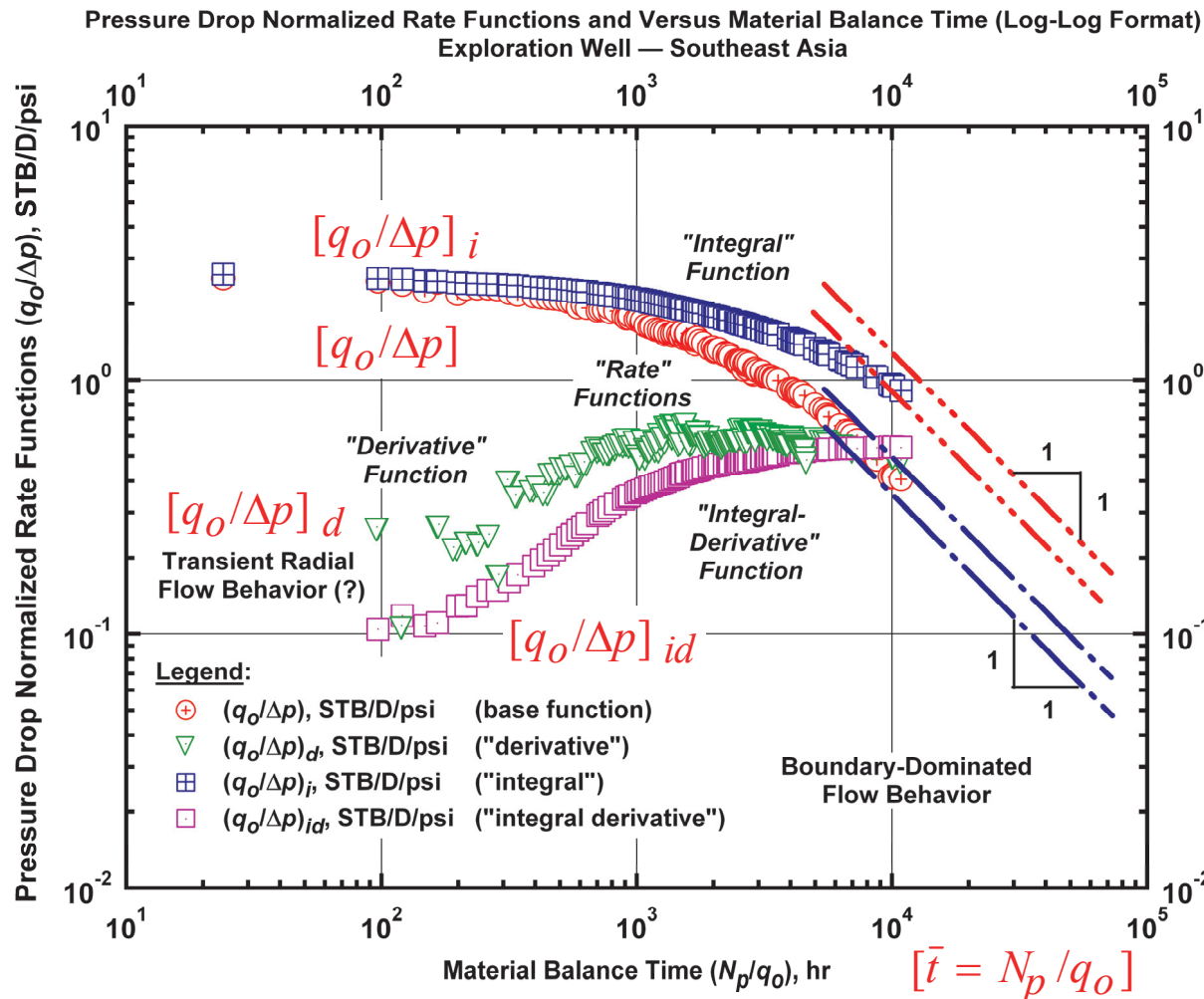
Discussion: Modern PA — Aux. Plotting Functions ("Normalized PI" plot)

- $(\Delta p/q_o)$ functions versus N_p/q_o ? (PTA form: transient flow — ?, BDFB — yes!)
- Validity of $(\Delta p/q_o)_d$ function? (exceptional case — downhole pressure data)
- $(\Delta p/q_o)_i$ and $(\Delta p/q_o)_{id}$ functions? (smooth and representative)

Auxiliary Plotting Functions (Application 2)

Q. Application 2 — What is the "Blasingame" plot?

A. Rate auxiliary functions versus material balance time.



Theory:

$(q_o/\Delta p)$ fcns versus N_p/q_o :

$$\bar{t} = \frac{N_p}{q_o}$$

$$\left[\frac{q_o}{\Delta p} \right]_d = \bar{t} \left| \frac{d}{d\bar{t}} \left[\frac{q_o}{\Delta p} \right] \right|$$

$$\left[\frac{q_o}{\Delta p} \right]_i = \frac{1}{\bar{t}} \int_0^{\bar{t}} \left[\frac{q_o}{\Delta p} \right] d\bar{t}$$

$$\left[\frac{q_o}{\Delta p} \right]_{id} = \bar{t} \left| \frac{d}{d\bar{t}} \left[\left[\frac{q_o}{\Delta p} \right]_i \right] \right|$$

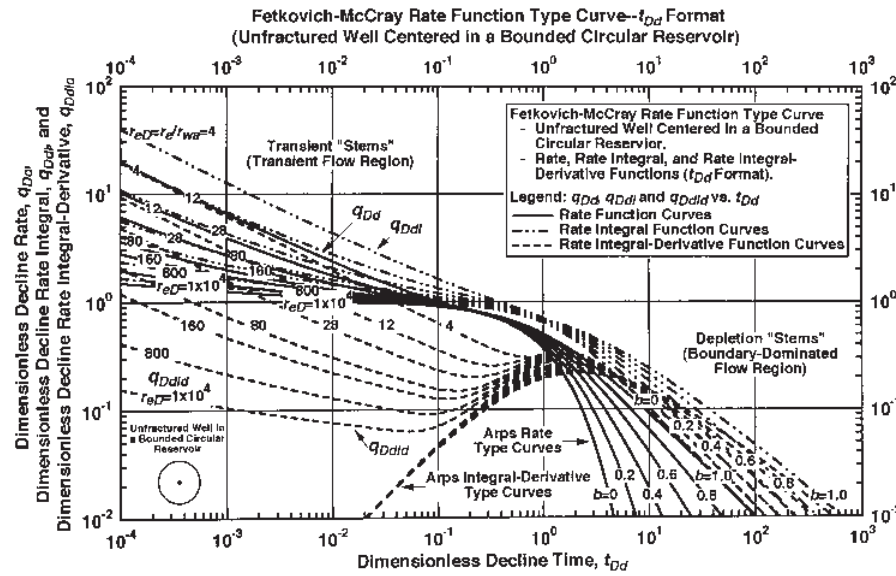
Application:

Transient flow behavior is complex, but transition and BDFB unique.

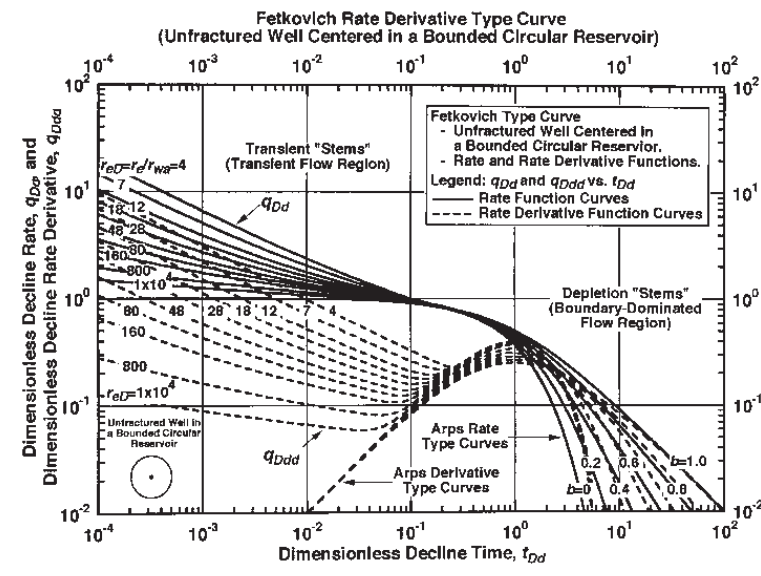
Discussion: Modern PA — Auxiliary Plotting Functions ("Blasingame" plot)

- $(q_o/\Delta p)$ versus N_p/q_o ? (rate decline form: transient flow — ?, BDFB — yes!)
- Validity of $(q_o/\Delta p)_d$ function? ((again) good — downhole pressure data)
- $(q_o/\Delta p)_i$ and $(q_o/\Delta p)_{id}$ functions? (well-behaved and representative)

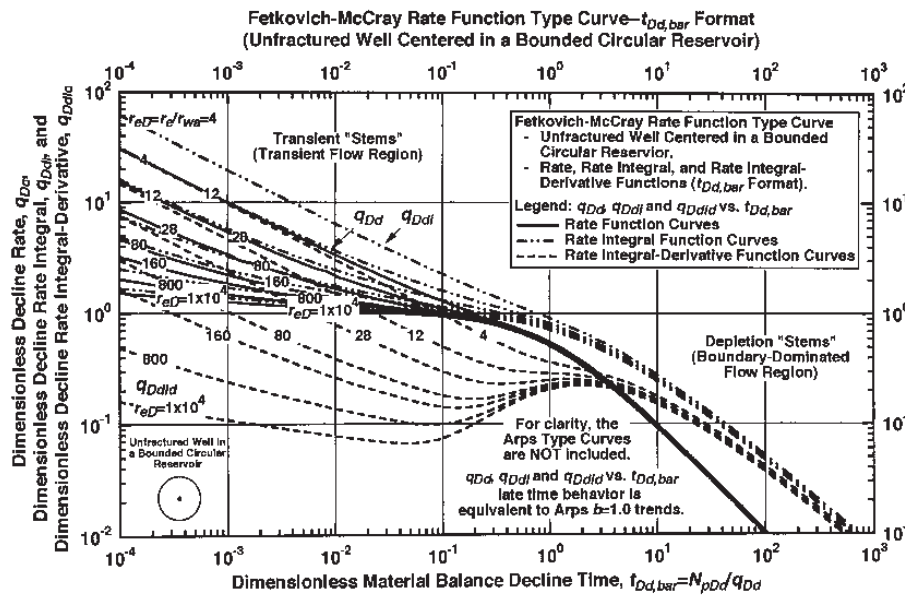
Fetkovich Radial Flow Type Curves



a. Palacio, et al (1993): "Fetkovich-McCray Original" (radial flow) — auxiliary functions. (t_{Dd} format)



b. Doublet, et al (1994): "Fetkovich Derivative" (radial flow) — not practical for analysis. (t_{Dd} format)



c. Doublet, et al (1994): "Fetkovich-McCray M.B. Time" (radial flow) — w/aux. functions. ($t_{Dd,bar}$)

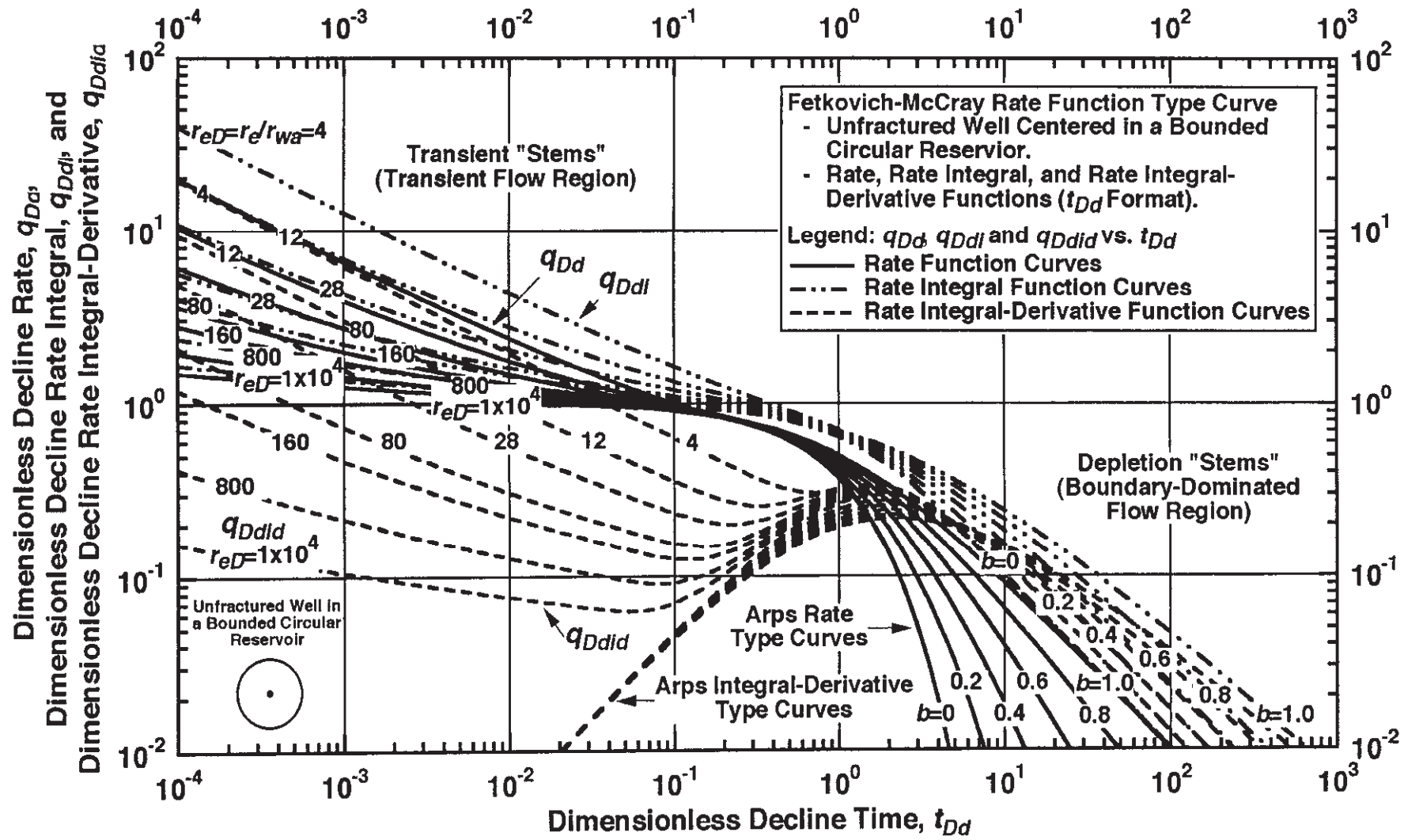
Radial Flow Decline TC:

- "Fetkovich-McCray Original"
- "Fetkovich Derivative"
- "Fetkovich-McCray Material Balance Time" — Uses material balance to rigorously incorporate variations in rate and pressure over time. This technique substantially improves the analysis of variable-rate data.

Doublet, L.E., Pande, P.K., McCollum, T.J., and Blasingame, T.A.: "Decline Curve Analysis Using Type Curves — Analysis of Oil Well Production Data Using Material Balance Time: Application to Field Cases," paper SPE 28688 presented at the 1994 Petroleum Conference and Exhibition of Mexico held in Veracruz, MEXICO, 10-13 October 1994.

Palacio/Blasingame Type Curve

Fetkovich-McCray Rate Function Type Curve- t_{Dd} Format
(Unfractured Well Centered in a Bounded Circular Reservoir)



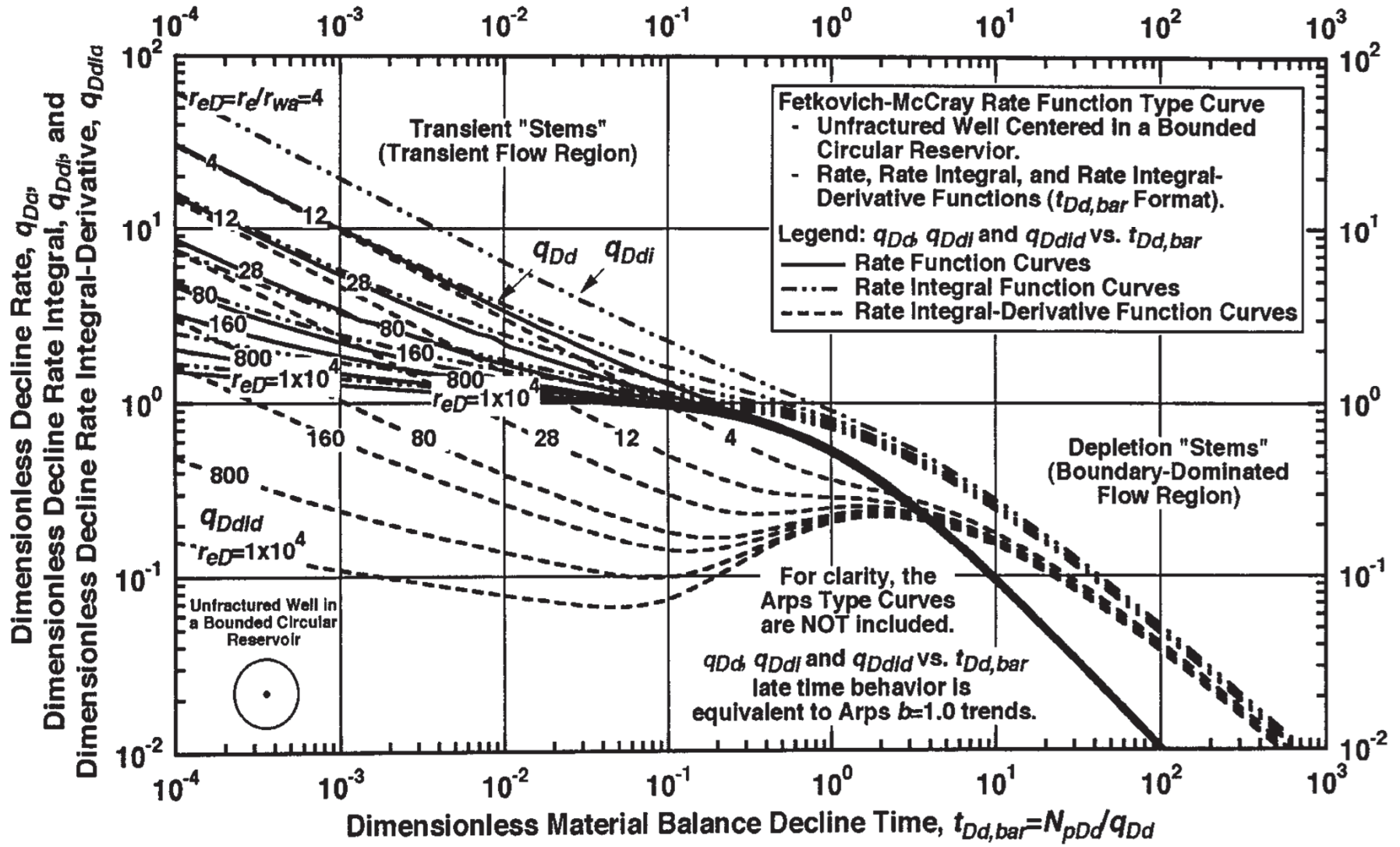
Discussion: Palacio/Blasingame Type Curve (constant p_{wf} case)

- Auxiliary functions (rate integral and integral derivative) enhance flow features.
- Need to use material balance time to account for variable rate.
- This plot includes the "Arps' relations," these are not included in general.

Palacio, J.C. and Blasingame, T.A.: "Decline Curve Analysis Using Type Curves — Analysis of Gas Well Production Data," paper SPE 25909 presented at the 1993 Joint Rocky Mountain Regional/Low Permeability Reservoirs Symposium, Denver, CO, 26-28 April 1993.

Doublet/Blasingame Type Curve

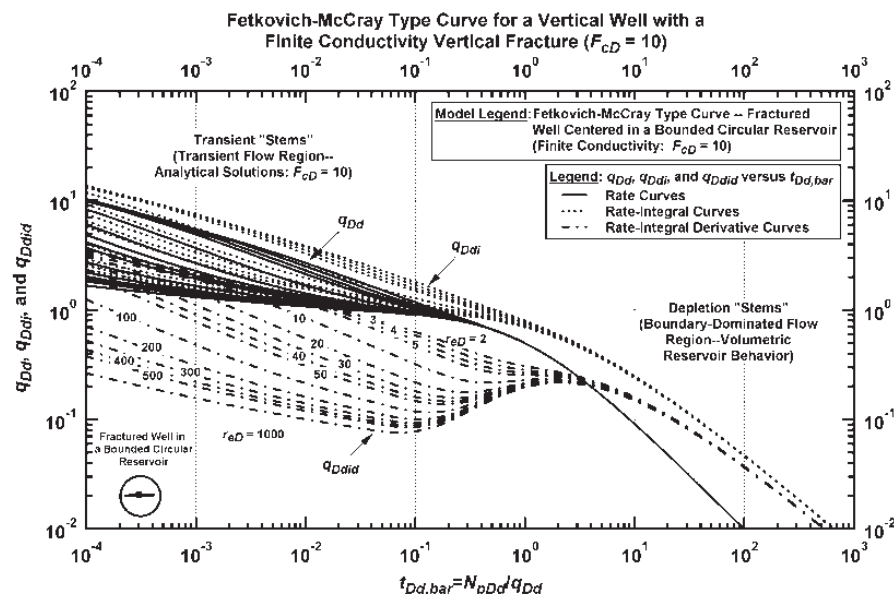
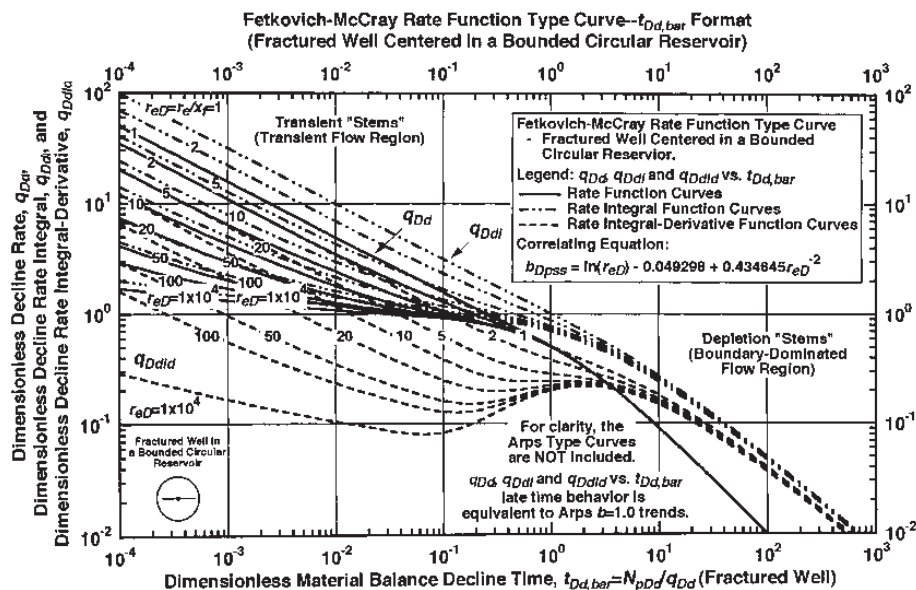
Fetkovich-McCray Rate Function Type Curve-- $t_{Dd,bar}$ Format
(Unfractured Well Centered in a Bounded Circular Reservoir)



Discussion: Doublet/Blasingame Type Curve (constant q_o equivalent)

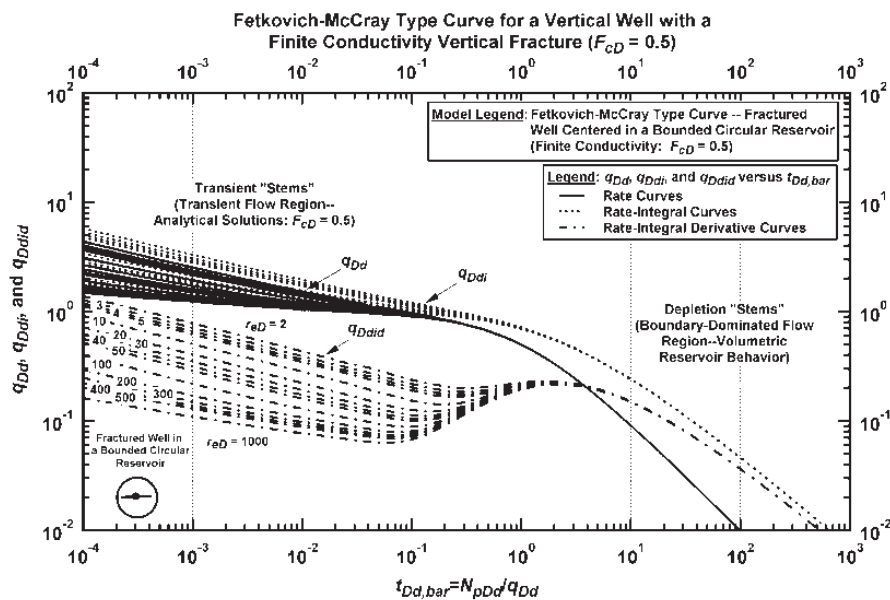
- Note "convergence" of late stems to unique trends (material balance time).
- Type curve is valid for variable-rate/variable pressure drop cases.
- Original "RTA" plot — there is a companion plot for rate normalized pressure.

Doublet/Blasingame Type Curve — Vertically Fractured Wells



a. Doublet, et al (1996): "Fetkovich-McCray" format — INFINITE conductivity vertical fracture ($F_{CD} = \infty$).

b. Pratikno (2002): "Fetkovich-McCray" format — FINITE conductivity vertical fracture ($F_{CD} = 10$).



c. Pratikno (2002): "Fetkovich-McCray" format — FINITE conductivity vertical fracture ($F_{CD} = 0.5$).

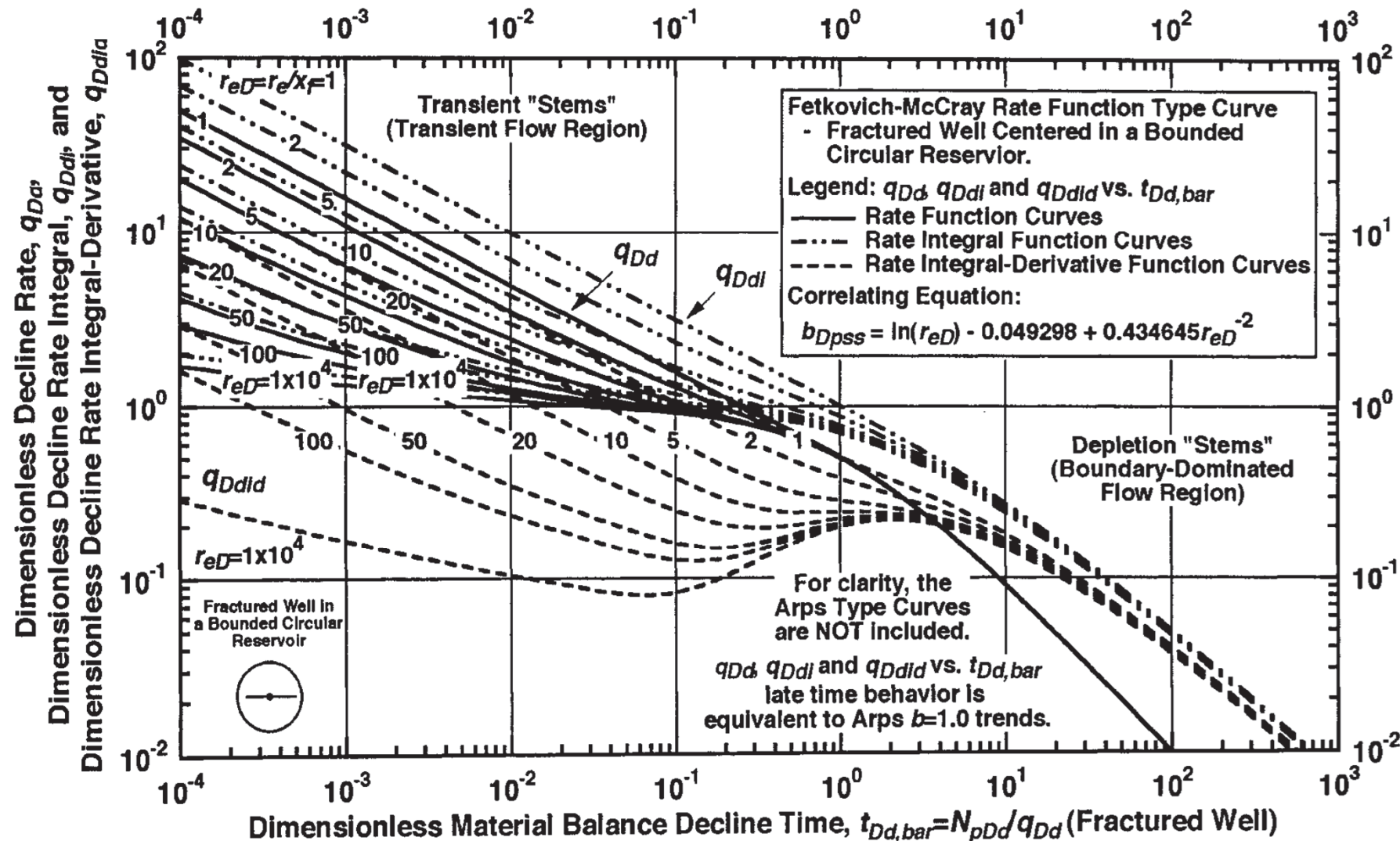
Decline Type Curves: Fractured Wells

- **Infinite fracture conductivity:**
 - Less complex solution, but somewhat ideal for use in practice.
- **Finite fracture conductivity:**
 - $F_{CD} = 10$: Moderate to high fracture conductivity case.
 - $F_{CD} = 0.5$: Low fracture conductivity case.

Pratikno, H., Rushing, J.A., and Blasingame, T.A.: "Decline Curve Analysis Using Type Curves: Fractured Wells," paper SPE 84287 presented at the 2003 Annual SPE Technical Conference and Exhibition, Denver, CO., 05-08 October 2003.

Doublet/Blasingame Type Curve Format — Vertically Fractured Wells

Fetkovich-McCray Rate Function Type Curve- $t_{Dd,bar}$ Format
(Fractured Well Centered in a Bounded Circular Reservoir)



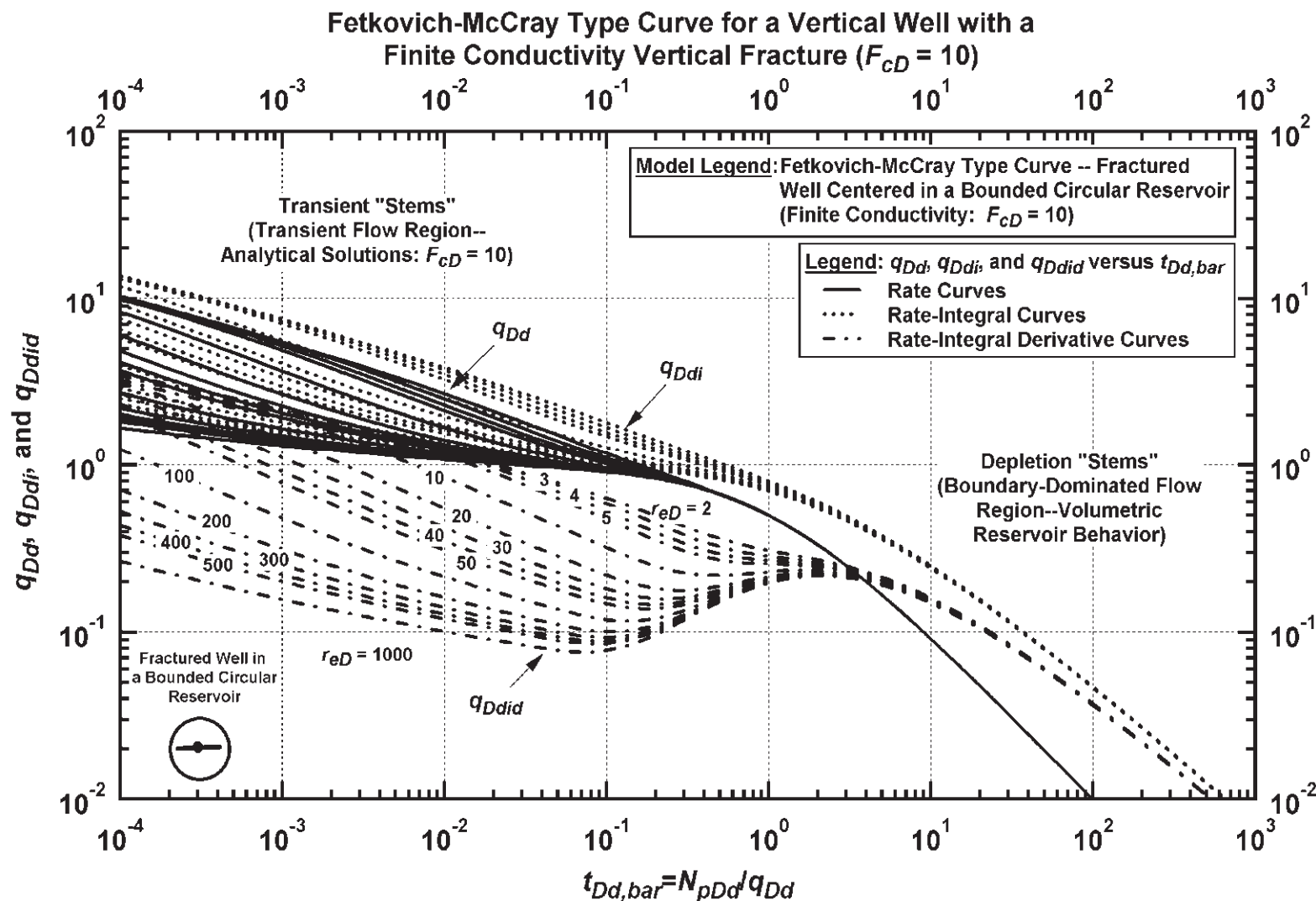
Discussion: Doublet/Blasingame Type Curve (infinite conductivity fracture)

- Note the transient flow behavior of the auxiliary functions (linear flow).
- Use of material balance time provides unique late time behavior.
- Can estimate fracture half-length, permeability, and reservoir volume.

Doublet, L.E. and Blasingame, T.A.: "Evaluation of Injection Well Performance Using Decline Type Curves," paper SPE 35205 presented at the 1996 SPE Permian Basin Oil and Gas Recovery Conference, Midland, TX, 27-29 March, 1996.

Doublet/Blasingame Type Curve Format — Vertically Fractured Wells

Pratikno, H., Rushing, J.A., and Blasingame, T.A.: "Decline Curve Analysis Using Type Curves: Fractured Wells," paper SPE 84287 presented at the 2003 Annual SPE Technical Conference and Exhibition, Denver, CO., 05-08 October 2003.

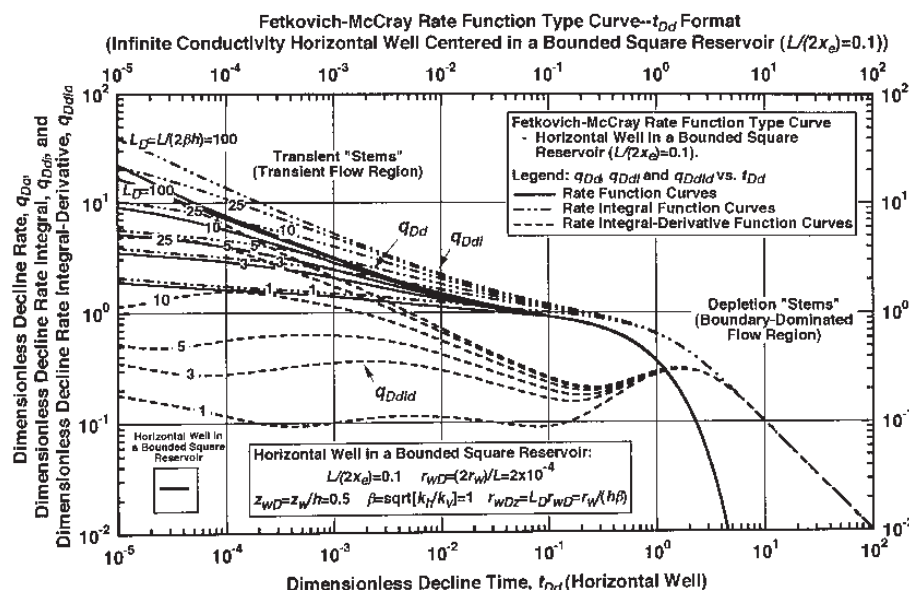
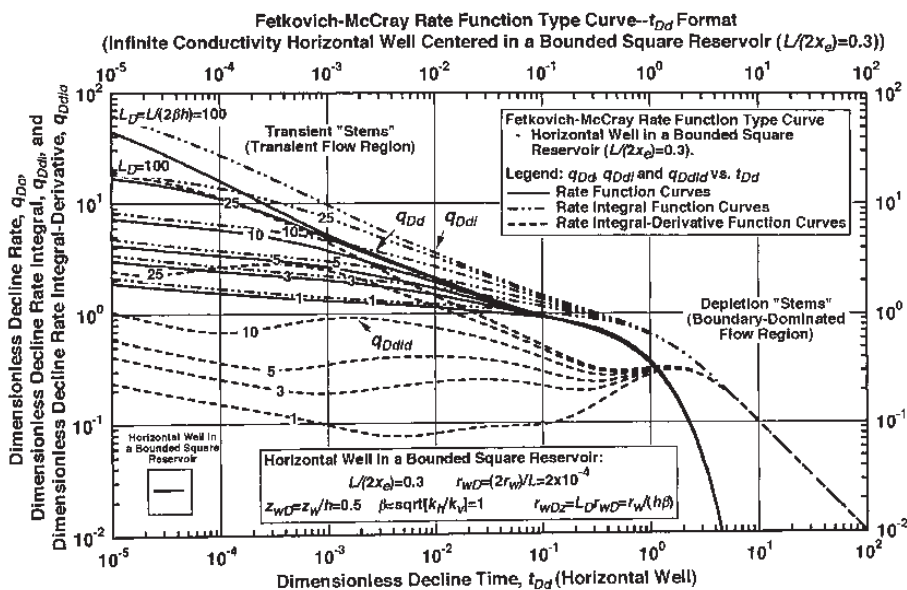
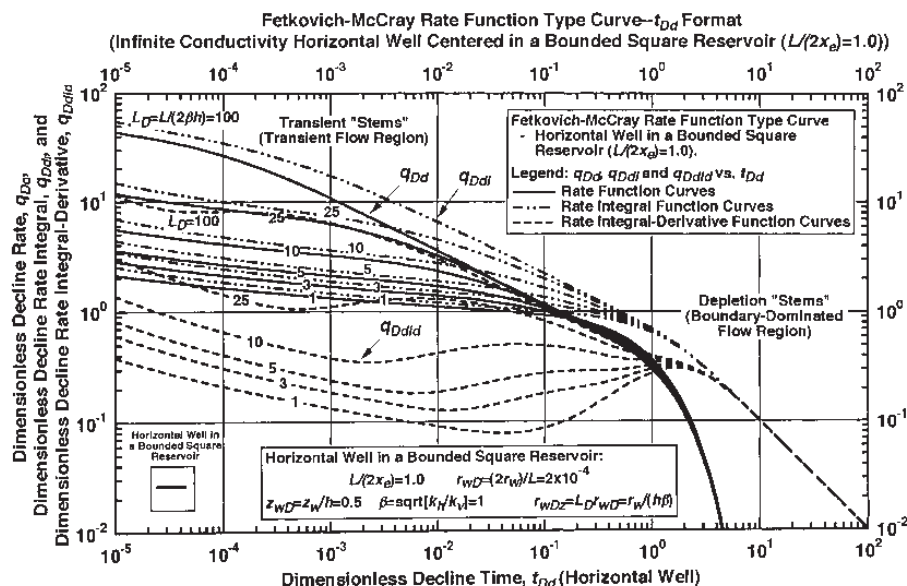


Discussion: Doublet/Blasingame Type Curve (Finite conductivity fracture)

- Note the transient flow behavior of the auxiliary functions (bilinear flow).
- Individual type curves generated for each F_{cD} -value.
- Can estimate fracture half-length, permeability, and reservoir volume.

Doublet/Blasingame Type Curve Format — Horizontal Wells

Shih, M.-Y. and Blasingame, T.A.: "Decline Curve Analysis Using Type Curves: Horizontal Wells," paper SPE 29572 presented at the 1995 Joint Rocky Mountain Regional/Low Permeability Reservoirs Symposium, Denver, CO, 20-22 March, 1995.

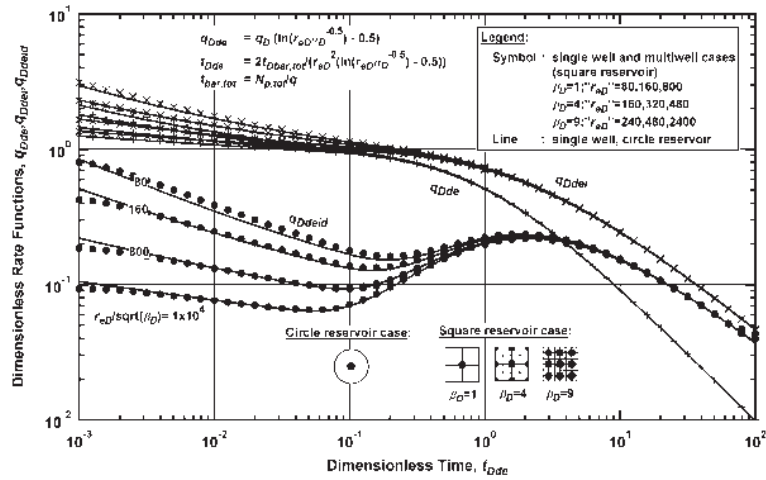


Horizontal Well Cases:

- "Infinite-conductivity" horizontal well case(s).
- Dimensionless reservoir model requires several parameters.

Decline Type Curves — Boundary Flux Cases

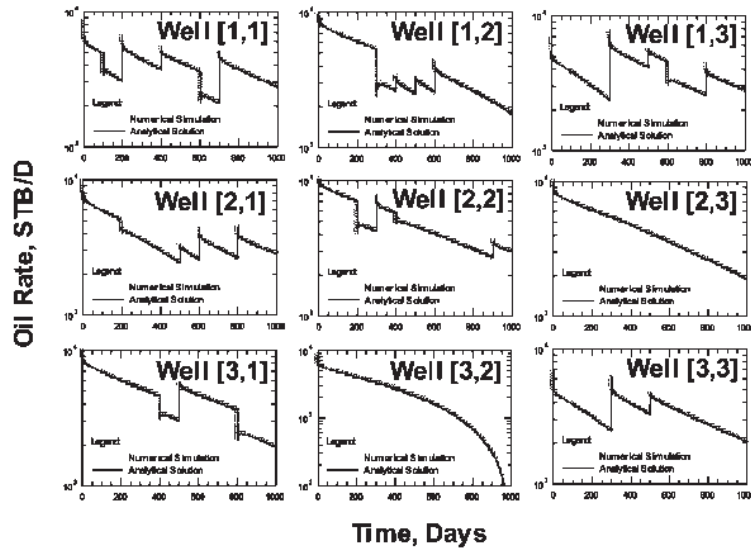
Marhaendrajana, T. and Blasingame, T.A.: "Decline Curve Analysis Using Type Curves — Evaluation of Well Performance Behavior in a Multiwell Reservoir System," paper SPE 71514 presented at the 2001 Annual SPE Technical Conference and Exhibition, New Orleans, 30 Sept.-03 Oct. 2001.



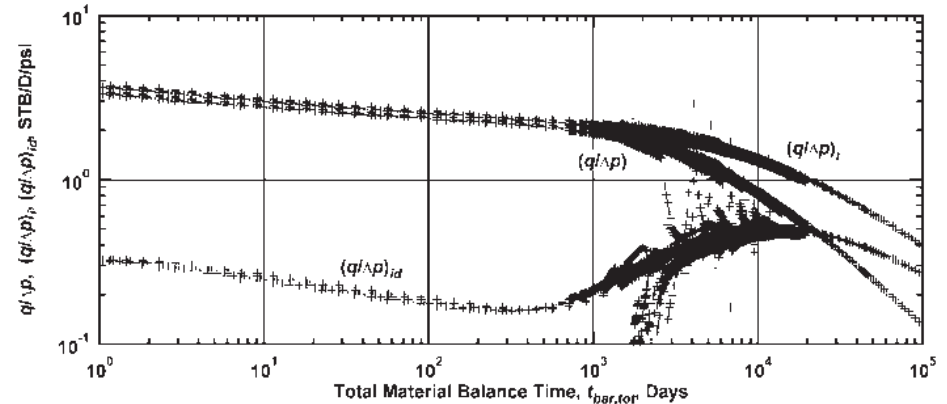
Dimensionless "decline variables" plot for the single well and multiwell performance cases — simulated performance used to validate the multiwell concept.

Multiwell Analysis: SPE 71514

- Multiwell case can be "recast" into single well case using cumulative production for entire field.
- Homogeneous reservoir example shows that all cases (9 wells) align — same behavior observed for heterogeneous reservoir cases.

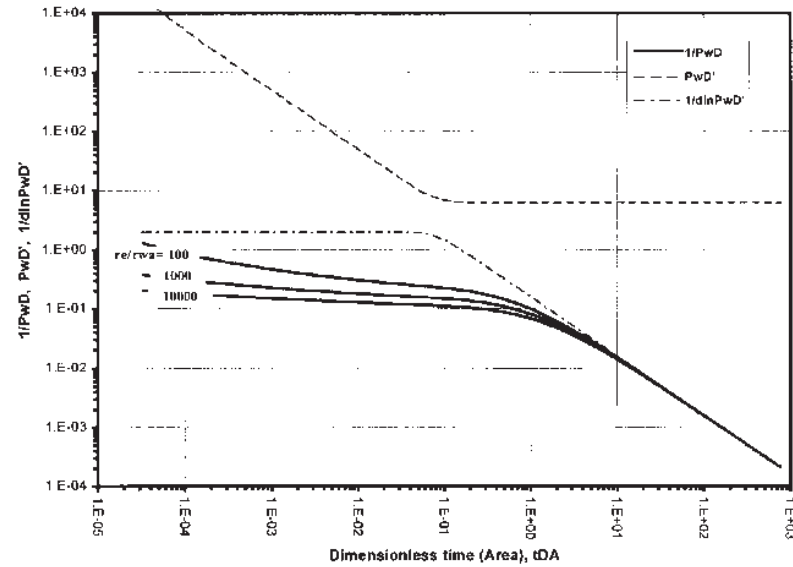


Oil rate versus time profiles (homogeneous reservoir example). (O Numerical Simulation, — Analytical Solution)



Log-log plot of rate/pressure drop functions as a function of total material balance time (homogeneous reservoir example).

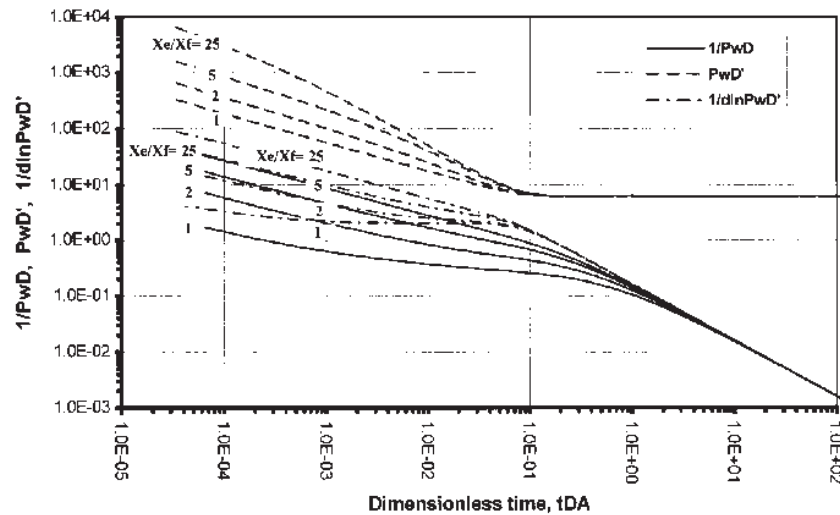
Decline Type Curves — Agarwal, et al Methodology



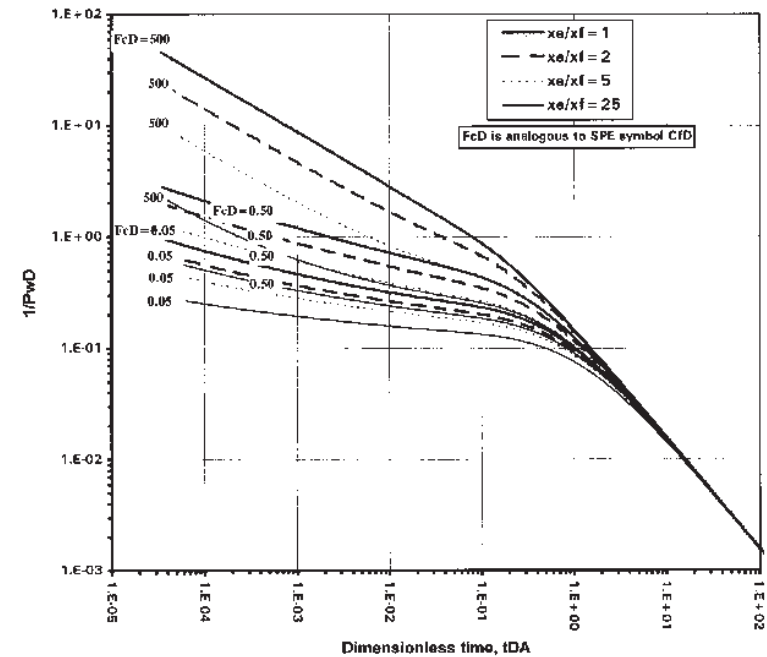
Rate-time production decline-type curves for radial systems using t_D based on area ($r_e/r_{wa} = 100, 1,000, 10,000$).

Agarwal, et al Methodology: SPE 57916

- Basically the same as Blasingame, et al work.
- More like pressure transient test analysis/interpretation.



Rate-time production decline-type curves for infinite conductivity fracture using t_D based on area ($x_e/x_f = 1, 2, 5, 25$).

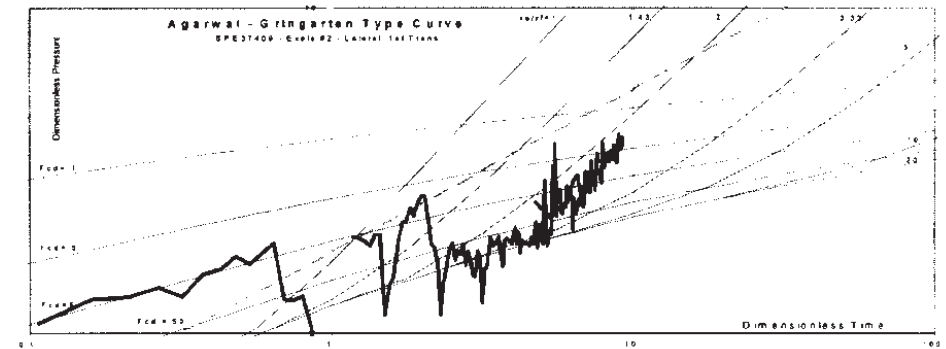
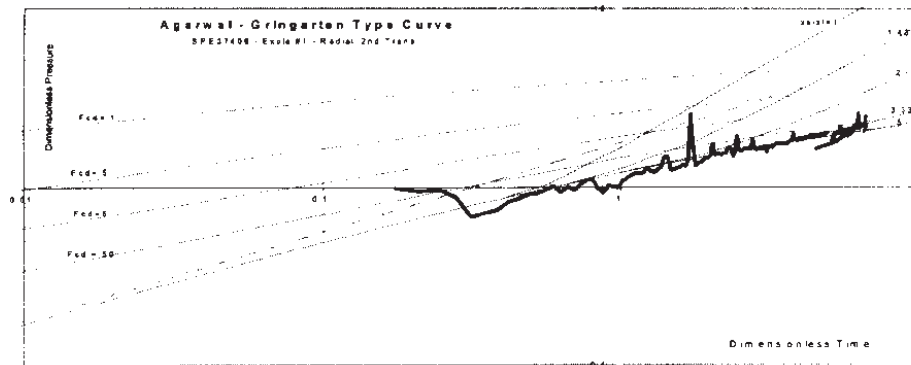
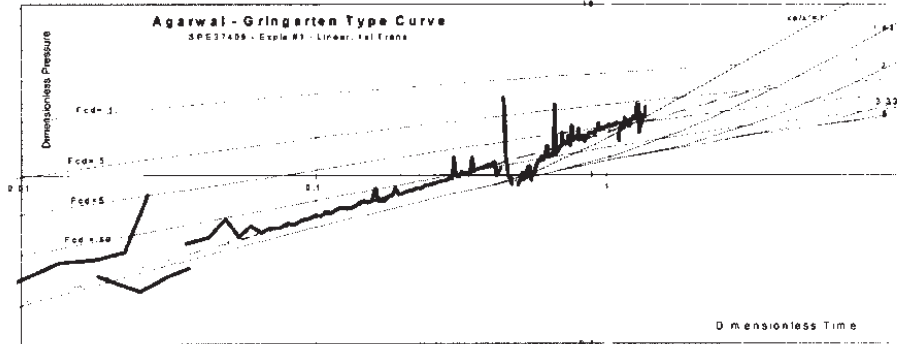


Rate-time production decline-type curves for finite conductivity fracture using t_D based on area ($x_e/x_f = 1, 2, 5, 25$ and $F_{cD} = 0.05, 0.5, 500$).

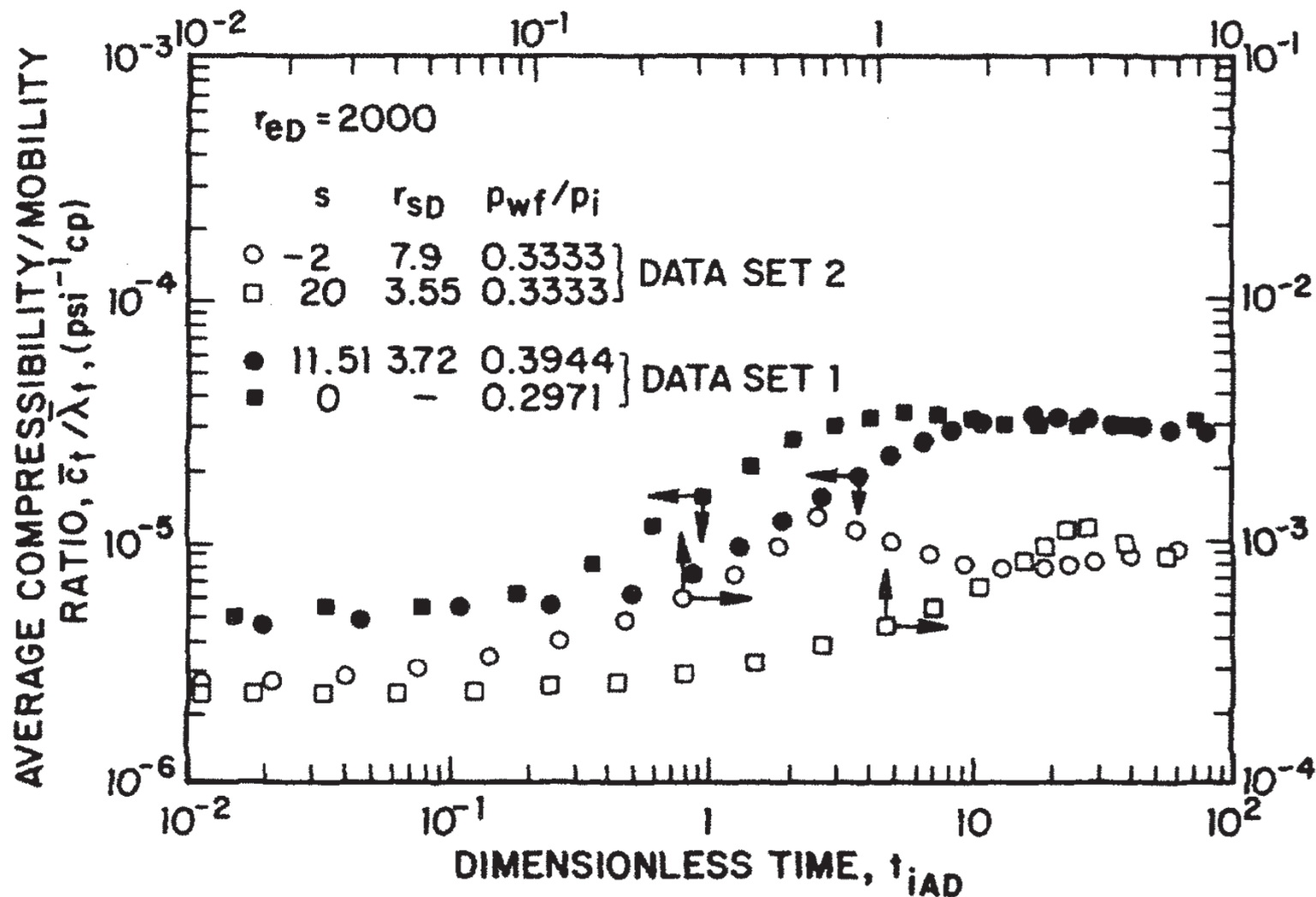
Crafton, et al Methodology

Crafton, et al Methodology: SPE 37409

- Rate normalized pressure drop versus production time ($\Delta p/q$ vs. t).
- Also analogous to pressure transient test analysis/interpretation.
- Very serious limitations — production time is not sufficient for general case of rate variation.



Single-Phase Liquid (Black Oil) — (c_f/λ_f) vs. Time



Variation of average compressibility/mobility ratio with time.

Discussion: "Solution-Gas Drive" Behavior — $((c_f/\lambda_f)$ vs. time)

- Observation: $(c_f/\lambda_f) \cong$ constant for $p > p_b$ and later, for $p < p_b$.
- p_{wf} = constant — but probably valid for any production/pressure scenario.

Camacho-V., R.G. and Raghavan, R.: "Boundary-Dominated Flow in Solution-Gas-Drive Reservoirs," SPE (November 1989) 503-512.

Multiwell Analysis — Governing Relation

$$\frac{q_k(t)}{(p_i - p_{wf})} = \frac{1}{\frac{1}{Nc_t} \frac{1}{q_k(t)} \int_0^t \sum_{i=1}^{n_{well}} q_i(t) dt + c(t)}$$

↑

**Production Data
(Pressure & Rate)**

↑

**Total Material
Balance Time**

||

$\bar{t}_{tot} = \frac{N_{p,field}}{q_{well}}$

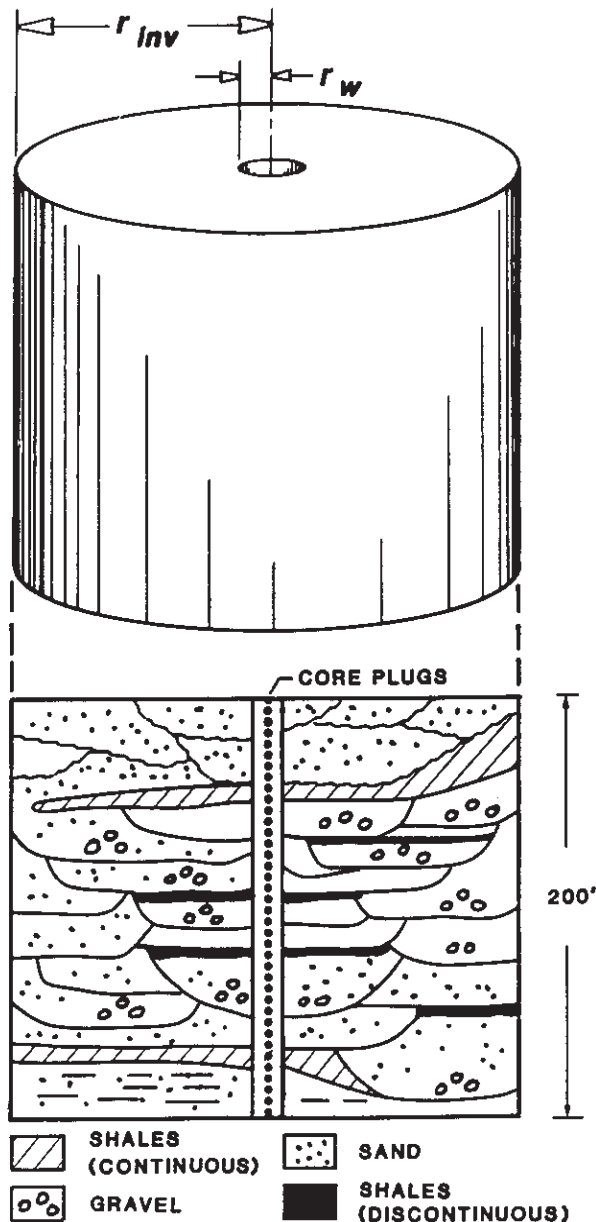
↑

**c(t) becomes constant at
long times**

Discussion: Multiwell Analysis — Governing Relation

- A general formulation of the "Arps' Exponential Decline" case.
- **CONCLUSION:** A single well decline type curve can be used to analyze the performance of a single well in a multiwell system.

Reality Check



From: Simulator Parameter Assignment and the Problem of Scaling in Reservoir Engineering — Halderson (1986).

Reservoir Volume-Averaging

- Pressure transient analysis.
- Production data analysis.
- Reservoir simulation.

Advanced Solutions

- Same view of the reservoir — just more "knobs" (*i.e.*, parameters).
- Time-pressure-rate data will always "see" a pressure/volume-averaged reservoir system.

Prediction of Future Work in PTA/PA

- Additional reservoir models.
- Full incorporation of PVT character.
- Reservoir scaling for PTA/PA.
- Handling poor quality data.
- Continuously measured p_{wf} data.
- Multiple well analysis/integration.
- Coupling of analysis/interpretation with numerical modeling (3D/3P).

References — Production Data Analysis

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